# VERTICAL MOTIONS OF SYNOPTIC SCALE 

Yu.L. Matveev and L.T. Matveev<br>Russian State Hydrometeorological Institute, St. Petersburg<br>Received May 7, 1998

Vertical motions observed in synoptic vortex (upward - in cyclone and downward - in anticyclone) have a primary influence on not only the formation and growth of clouds, but also spread of admixtures of both natural and anthropogenic origin, as well as levels of air pollution near the Earth's surface. The influence of such parameters as geostrophic and surface wind, surface roughness, thermodynamic stability of the ground layer of the atmosphere, and the horizontal size of vortex on the vertical velocity was estimated using equations of the similarity theory. The results are presented as tables, which allow calculation of the vertical velocity at any level of the boundary layer using the data of synoptic maps. A good agreement of results (in the boundary layer) on vertical velocity calculation within the framework of the similarity theory and using the equation approximating the vertical velocity within the entire troposphere suggests that the latter equation can be used in modeling of the atmospheric processes and phenomena.

In a number of studies, ${ }^{1,2}$ it was shown that vertical motions of synoptic scale play a leading part in formation of not only stratus ( $N s-A s-C s$ ), but also stratocumulus ( $\mathrm{Cu}, \mathrm{Cb}$ ) clouds.

In this case, to model the $N s-A s$ clouds, it is sufficient to know that air executes an upward motion ( $w>0$ ). Certainly, the time of formation, the height of borders, and the profile of clouds depend significantly on the height distribution of vertical velocity ( $w$ ), temperature ( $T$ ), and the water vapor mass fraction ( $q$ ) at the initial moment, as well as the turbulent exchange intensity, etc. Nevertheless, early or late, high or low, a cloud will necessarily be formed at $w>0$.

Vertical motions of the synoptic scale also play the decisive part in the convective clouds ( $C u, C b$ ) formation. However, in contrast to $N s-A s$, when modeling the convective clouds it is a prime necessity to take into account not only the sign, but also the height distribution of $w$. The vertical temperature lapse rate $(\gamma=-\partial T / \partial z)$ varies with time in response to $w$ change with increasing altitude.

Vertical motions in the atmospheric boundary layer (ABL) are most completely studied. ${ }^{3,4}$ In one of the recent papers in this line, ${ }^{5}$ the model of height distribution of $w$ was constructed, which takes into account (within the framework of the similarity theory) sufficiently fine features of ABL structure.

Using the equations of continuity and steady motion, it was shown in Ref. 4 that for the vertical velocity averaged over some area $\sigma$
$\bar{w}=\frac{1}{\sigma} \iint_{(\sigma)} w \mathrm{~d} \sigma$
the following expression is valid
$\bar{\omega}(z)=\frac{1}{2 \omega_{z} \rho \sigma} \int_{(l)}\left(\tau_{0 l}-\tau_{l}\right) \mathrm{d} l$.
Here $l$ is the contour enclosing the area $\sigma ; \tau_{l}$ and $\tau_{0 l}$ are the $l$ projections of the turbulent stress at a height $z$ and on the Earth's surface ( $z=0$ ), respectively; $2 \omega_{z}$ is Coriolis parameter; $\rho$ is an air density.

At the top of the boundary layer ( $H$ ) where $\tau_{l}$ is close to zero, Eq. (1) takes the form
$\bar{w}(H)=\frac{1}{2 \omega_{z} \rho_{H} \sigma} \int_{(l)} \tau_{0 l} \mathrm{~d} l$.
Expression for $\tau_{l}$ is obtained in Ref. 5
$\tau_{0 l} /\left(2 \omega_{z} \rho_{H}\right)=c_{g} z_{1} G / 2 ;$
$G=\sqrt{\frac{c_{1}}{c_{g}} D \operatorname{Ro}} \times\left[1-B \frac{c_{1}}{c_{g}}\left(\cos \alpha_{0}-\sin \alpha_{0}\right)\right]$,
where $c_{g}$ is velocity of the geostrophic wind; $c_{1}$ is the absolute value of the wind velocity at the level $z_{1} ; z_{0}$ is the surface roughness parameter; $\mathrm{Ro}=c_{g} /\left(\omega_{z} \cdot z_{1}\right)$ is an analog of the Rosbi parameter; $\alpha_{0}$ is the deflection angle of the wind velocity vector near the Earth's surface from the tangent to isobar (direction of the geostrophic wind) determined by the expression
$\cos \alpha_{0}=\frac{1+B^{2}\left(c_{1} / c_{g}\right)^{2}-\operatorname{Ro} N\left(c_{1} / c_{g}\right)^{3}}{2 B\left(c_{1} / c_{g}\right)} ;$
$B, D$, and $N$ are the dimensionless parameters depending on ratios $z_{0} / z_{1}$ and $z_{1} / z ; L$ is the scale of the Monin-Obukhov ground layer; values of these parameters are tabulated in Ref. 5.

On the assumption that the area $\sigma$, over which the average value $\bar{w}$ is determined, is the circle of radius $r$, and parameters entering into Eqs. (3) and (4) weakly vary along the $l$ contour, Eq. (2) takes the following form:
$\bar{w}(H)=c_{g} z_{1} \cdot G / r$.
At fixed thermal stability and roughness of the Earth's surface (i.e., $L / z_{1}$ and $z_{0} / z_{1}$ ), the angle $\alpha_{0}$ and the parameter $G$ grow as Ro and $c_{1} / c_{g}$ increase. Thus, at $L / z_{1}=50, z_{0} / z_{1}=0.1$ and $c_{1} / c_{g}=0.5$ we have the following $\alpha_{0}$ and $G$ values for different Ro:

| $10^{-4}$ Ro | 2 | 3 | 4 | 5 | 6 | 8 | 10 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $\alpha_{0}, \operatorname{degs}$ | 27 | 36 | 41 | 45 | 50 | 55 | 62 |
| $G$ | 94 | 132 | 170 | 220 | 292 | 400 | 550 |

At $L / z_{1}=20, z_{0} / z_{1}=0.1$ and Ro $=2 \cdot 10^{4}, \alpha_{0}$ and $G$ values for different $c_{1} / c_{g}$ are the following:

| $c_{1} / c_{g}$ | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| :--- | :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| $\alpha_{0}$, degs | 11 | 20 | 30 | 38 | 45 | 51 | 56 | 66 | 76 |
| $G$ | 12 | 24 | 48 | 72 | 98 | 122 | 146 | 196 | 246 |

At fixed dynamic parameters ( $\mathrm{Ro}=3 \cdot 10^{4}$ and $\left.c_{1} / c_{g}=0.4\right)$ and surface roughness $\left(z_{0} / z_{1}=0.1\right)$, the angle $\alpha_{0}$ and $G$ increase as $L / z_{1}$ decreases, i.e. as the ground layer stability increases:

| $L / z_{1}$ | 50 | 20 | 10 |
| :--- | :---: | :---: | :---: |
| $\alpha_{0}$ | 31 | 54 | 88 |
| $G$ | 90 | 120 | 126 |

It is easily seen that the influence of different parameters on $\alpha_{0}$ and $G$ is determined by their influence on the friction stress $\left(\tau_{0}\right)$ near the Earth's surface. Indeed, since
$\sqrt{\tau_{0} / \rho_{0}}=u_{*}=x\left(c_{1} / c_{g}\right) c_{g} / \ln \left(\eta_{1} / \eta_{0}\right)$
and
$\frac{\eta_{1}}{\eta_{0}}=\frac{z_{1}}{z_{0}}\left(1+\frac{z_{1}}{2 L}+\frac{z_{1}^{2}}{6 L^{2}}+\ldots\right)$,
then:

1) at fixed $c_{g}, c_{1} / c_{g}$, and $z_{1} / L$, increase in $z_{0} / z_{1}$ leads to growth of $\tau_{0}$ and, as a consequence, to an increase of $\alpha_{0}$ and $G$;
2) at fixed $z_{0} / z_{1}$, and $z_{1} / L$, decrease in $c_{g}$ or $c_{1} / c_{g}$ is followed by decrease in $\tau_{0}$ along with decrease in $\alpha_{0}$ and $G$;
3) at fixed $c_{g}, c_{1} / c_{g}$, and $z_{0} / z_{1}$, increase in $L / z_{1}$, i.e. approaching the neutral stratification, leads to growth of $\tau_{0}, \alpha_{0}$, and $G$. However, in this case, in addition to $\tau_{0}$, the altitude of the ground layer ( $h$ ) influences the deflection angle ( $\alpha$ ) too. It is obvious that the higher is the $h$ level, the closer is the wind at this level to the geostrophic wind, i.e., the less is $\alpha$.

Since within the ground layer the angle $\alpha$ varies only slightly with increasing altitude ( $\alpha_{h} \approx \alpha_{0}$ ), and the altitude of the ground layer is accepted to be $|L|$, the growth of $L$ under the effect of altitude increase leads to decrease in $\alpha_{0}$. The above data testify that this second effect is more essential than the influence of $\tau_{0}$ : as $L$ increases, the angle $\alpha_{0}$ decreases.

Transformation from strongly stable $\left(L / z_{1}<10\right)$ to strongly unstable $\left(L / z_{1}>-10\right)$ stratification is followed by growth of the turbulent exchange intensity, as well as strengthening of the interaction between the ground layer and the upper part of the boundary layer and, as a consequence, decrease in the deflection angle $\alpha_{0}$ (Table I).

Let us point out that at $L / z_{1}$ values exceeding $30-50$, when the thermal stratification is close to neutral, the dimensionless parameters entering Eqs. (3) and (4) can be written to sufficiently high accuracy in the form:
$B=\ln \left(\beta \frac{L}{z_{1}} \frac{z_{1}}{z_{0}}\right) / \ln \left(\frac{z_{1}}{z_{0}}\right) ;$
$D=\varkappa^{2} \beta \frac{L}{z_{1}} / \ln \left(\frac{z_{1}}{z_{0}}\right)$;
$N=\frac{1}{2} \frac{\chi^{2}}{\beta} / \ln ^{3}\left(z_{1} / z_{0}\right)$,
$\beta=(e-1) / e$ at $\gamma<\gamma_{a}$ and $\beta=1-e$ at $\gamma>\gamma_{a}$,
$e=2.7128 \ldots$.
It follows from the data presented in Table I that all the four parameters: Ro, $c_{1} / c_{g}, z_{0} / z_{1}$, and $L / z_{1}$ essentially influence the deflection angle. In this case, $\alpha_{0}$ varies widely from $5-10$ to $80-90^{\circ}$.

The results of calculation of the parameter $G$ derived in Ref. 4 are presented in Table II. Like the angle $\alpha_{0}$, the parameter $G$ varies widely depending on Ro, $c_{1} / c_{g}$, and $z_{0} / z_{1}$. An increase in each of these parameters leads to the growth of $G$. However, the parameter $G$ depends on the $L / z_{1}$ ratio far more weakly than $\alpha_{0}$ does.

Vertical velocity in the boundary layer most strongly depends on the geostrophic velocity (pressure gradient). At Ro $=4 \cdot 10^{4}, z_{0} / z_{1}=0.1, L / z_{1}=50$ and $c_{1} / c_{g}=0.5$, the parameter $G$ equals 170 according to the data from Table II.

TABLE I. Deflection angle $\alpha_{0}$ (degrees) at strongly unstable ( $L / z_{1}=-10$, numerator) and stable $\left(L / z_{1}=+10\right.$, denominator) thermal stratification of the ground layer.

| $10^{-4} \mathrm{Ro}$ | $c_{1} / c_{g}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| $z_{0} / z_{1}=0.01$ |  |  |  |  |  |  |  |  |  |
| 3 |  |  | -/8 | -/21 | $-/ 29$ | $-/ 35$ | $-/ 41$ | 15/49 | $24 / 57$ |
| 4 | -/11 | -/20 | 11/32 | 20/40 | $26 / 48$ | 30/54 | 34/60 | 42/71 | 48/81 |
| 5 | 10/20 | 17/29 | 26/42 | $32 / 51$ | $38 / 60$ | 43/68 | 48/76 | 56/- | 63/- |
| 6 | $16 / 23$ | $23 / 33$ | 32/48 | 40/61 | 46/71 | $52 / 81$ | 57/- | 67/- | 78/- |
| 8 | 17/23 | $25 / 36$ | 36/54 | 45/68 | $53 / 82$ | 60/- | 66/- | 78/- | 90/- |
| 10 | $14 / 22$ | $25 / 38$ | $39 / 60$ | $50 / 77$ | 58/- | 67/- | 74/- | 89 / - | -/- |
| $z_{0} / z_{1}=0.1$ |  |  |  |  |  |  |  |  |  |
| 2 | -/3 | -/25 | -/43 | $24 / 57$ | $34 / 69$ | 42/79 | 49/90 | 62/- | 73/- |
| 3 | 14/32 | 27/47 | 43/69 | 55/88 | 65/- | $75 / 17$ | 84/- | -/- | -/- |
| 4 | 28/41 | 41/60 | 59 / - | 75 / - | 89 / - |  |  |  |  |
| 5 | 34/47 | 49/72 | 73/- |  |  |  |  |  |  |
| 6 | 38/53 | $57 / 84$ | 86/- |  |  |  |  |  |  |
| 8 | 40/58 | 64/- |  |  |  |  |  |  |  |
| 10 | $43 / 65$ | 71/- |  |  |  |  |  |  |  |

TABLE II.

| Parameter $G$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $10^{-4} \mathrm{Ro}$ | $L / z_{1}$ | $c_{1} / c_{g}$ |  |  |  |  |  |  |  |  |
|  |  | 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 |
| $z_{0} / z_{1}=0.01$ |  |  |  |  |  |  |  |  |  |  |
| 3 | 10 | - | - | 18 | 31 | 42 | 53 | 63 | 84 | 106 |
|  | -10 | - | - | - | - | - | - | - | 80 | 105 |
| 4 | 10 | 8 | 17 | 33 | 49 | 66 | 82 | 99 | 133 | 165 |
|  | - 10 | - | - | 32 | 52 | 69 | 87 | 104 | 139 | 174 |
| 5 | 10 | 10 | 21 | 44 | 68 | 93 | 118 | 142 | - | - |
|  | - 10 | 12 | 25 | 49 | 73 | 98 | 123 | 148 | 198 | 249 |
| 6 | 10 | 11 | 25 | 57 | 91 | 126 | 161 | - | - | - |
|  | - 10 | 14 | 29 | 60 | 93 | 127 | 162 | 197 | 268 | 339 |
| 8 | 10 | 9 | 29 | 72 | 119 | 166 | - | - | 351 | - |
|  | -10 | 11 | 29 | 70 | 114 | 160 | 207 | 255 |  | 445 |
| 10 | 10 | 6 | 32 | 91 | 152 | - | - | - | - | - |
|  | - 10 | 5 | 28 | 81 | 138 | 199 | 261 | 324 | 447 | - |
| $z_{0} / z_{1}=0.1$ |  |  |  |  |  |  |  |  |  |  |
| 2 | 50 | 12 | 24 | 48 | 71 | 94 | 117 | 141 | 189 | 238 |
|  | 10 | 9 | 23 | 47 | 70 | 94 | 116 | 138 | - | - |
| 3 | 50 | 2 | 17 | 52 | 91 | 132 | 174 | 218 | 308 | 401 |
|  | 10 | 20 | 41 | 83 | 125 | - | - | - | - | - |
| 4 | 50 | - | - | 35 | 100 | 170 | 242 | 318 | 472 | 630 |
|  | 10 | 28 | 62 | - | - | - | - | - | - | - |
| 5 | 50 | - | - | - | 106 | 219 | 337 | 457 | 601 | 942 |
|  | 10 | 37 | 89 | - | - | - | - | - | - | - |
| 6 | 50 | - | - | - | 118 | 293 | 470 | 649 | 1002 | - |
|  | 10 | 48 | 123 | - | - | - | - | - | - | - |
| 8 | 50 | - | - | - | 145 | 400 | 654 | 905 | - | - |
|  | 10 | 63 | - | - | - | - | - | - | - | - |
| 10 | 50 | - | - | - | 196 | 550 | 895 | - | - | - |
|  | 10 | 82 | - | - | - | - | - | - | - | - |

Setting $z_{1}=10 \mathrm{~m}$ and $r=500 \mathrm{~km}$, we obtain the following values of $\bar{w}(H)$ at different $c_{q}$ :

| $c_{g}, \mathrm{~m} / \mathrm{s}$ | 5 | 10 | 15 | 20 | 25 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $\bar{w}(H), \mathrm{cm} / \mathrm{s}$ | 1.7 | 3.4 | 5.1 | 6.8 | 8.5 |

If the ratio $c_{1} / c_{g}=0.8$ at the same Ro, $z_{0} / z_{1}$, $L / z_{1}, z_{1}$, and $r$ values, then

| $c_{g}, \mathrm{~m} / \mathrm{s}$ | 5 | 10 | 15 | 20 | 25 |
| :--- | :--- | :--- | :--- | :--- | :--- |
| $\bar{w}(H), \mathrm{cm} / \mathrm{s}$ | 4.7 | 9.4 | 14.2 | 18.9 | 23.5 |

Let us note that at given Ro the velocity $c_{g}$ at the given latitude cannot exceed the value equal to
$\left(c_{g}\right)_{\text {max }}=7.29 \cdot 10^{-5} \sin \varphi z_{1}$ Ro.
This maximum value grows as $\varphi$ increases. On the other hand, the parameter Ro at observed $c_{g}$ values can reach the greater values, the smaller is the latitude. Thus, at the latitude $10^{\circ}$, as $c_{g}$ varies from 10 to $40 \mathrm{~m} / \mathrm{s}$, the parameter Ro increases from $7.9 \cdot 10^{4}$ to $3.2 \cdot 10^{5}$.

Even at $\quad \operatorname{Ro}=10^{5}, \quad L / z_{1}=50 ; \quad z_{0} / z_{1}=0.1 ;$ $c_{1} / c_{g}=0.6 ; r=500 \mathrm{~km}$, the vertical velocity $\bar{w}(H)$ increases from $8.9 \mathrm{~cm} / \mathrm{s}$ at $c_{g}=5 \mathrm{~m} / \mathrm{s}$ to $71.6 \mathrm{~cm} / \mathrm{s}$ at $c_{g}=40 \mathrm{~m} / \mathrm{s}$.

In tropical cyclones, $w(H)$ reaches particularly large values. Since the velocity of the geostrophic wind in them amounts up to $30-80 \mathrm{~m} / \mathrm{s}$, whereas the latitude is, as a rule, less than $20^{\circ}$, the parameter Ro can take values exceeding (3-5) $10^{5}$.

Thus, at the latitude $20^{\circ}$ at $c_{g} \approx 25 \mathrm{~m} / \mathrm{s}$, the parameter Ro $\approx 10^{5}$. Since, as follows from Table II, as Ro doubles, the parameter $G$ increases $2-3$ times, we obtain the following estimations for $\bar{w}(H)$ at the same $\varphi=20^{\circ}$ :
at $\quad z_{0} / z_{1} \approx 0.01, \quad c_{1} / c_{g}=0.5 ; \quad L / z_{1}=-10$, $r=200 \mathrm{~km}$
$\Rightarrow c_{g}=25 \mathrm{~m} / \mathrm{s}, \operatorname{Ro}=10^{5}, G \approx 200$, $\bar{\omega}(H) \approx 25 \mathrm{~cm} / \mathrm{s}$;
b) $c_{g}=75 \mathrm{~m} / \mathrm{s}, \operatorname{Ro}=3 \cdot 10^{5}, G \approx 500$, $\bar{w}(H)=1.88 \mathrm{~m} / \mathrm{s} ;$
at $\quad z_{0} / z_{1} \approx 0.1, \quad c_{1} / c_{g}=0.5 ; \quad L / z_{1}=50 \quad$ and $r=200 \mathrm{~km}$
$\Rightarrow c_{g}=25 \mathrm{~m} / \mathrm{s}, \operatorname{Ro}=10^{5}, G=550$, $\bar{\omega}(H)=69 \mathrm{~cm} / \mathrm{s}$;
b) $c_{g}=75 \mathrm{~m} / \mathrm{s}, \mathrm{Ro}=3 \cdot 10^{5}, G=1375$, $\bar{w}(H)=5.16 \mathrm{~m} / \mathrm{s}$.

At lesser latitude, values of $\bar{w}(H)$ may be even more considerable (at the latitude of $10^{\circ}$, for example,
the above-presented values of $\bar{w}(H)$ are nearly doubled).

The obtained estimations of $\bar{w}(H)$ should be taken into account when modeling the tropical cyclones. It is known that, in an attempt to obtain the $w$ values about $10^{0}-10^{1} \mathrm{~m} / \mathrm{s}$, researchers arbitrarily invoke some additional vertical velocity, which is absolutely inconsistent with the solution of the set of equations.

The vertical velocity $\bar{w}(H)$ at an arbitrary altitude $z$, being averaged over the same area $\sigma=\pi r^{2}$, is calculated in accordance with Ref. 1 using the equations
$\bar{w}(z)=c_{g} z_{1}\left(G-G_{z}\right) / r+\bar{w}_{h} ;$
$G_{z}=\sqrt{\frac{c_{1}}{c_{g}} D \operatorname{Ro}}\left\{\left[1-B \frac{c_{1}}{c_{g}}\left(\cos \alpha_{0}-\sin \alpha_{0}\right)\right] \times\right.$
$\times \cos \frac{a}{z_{1}}(z-h)+\left[1-B \frac{c_{1}}{c_{g}}\left(\cos \alpha_{0}+\sin \alpha_{0}\right)\right] \times$
$\left.\times \sin \frac{a}{z_{1}}(z-h)\right\} \exp \left[-\frac{a}{z_{1}}(z-h)\right]$,
where $a=\sqrt{c_{g} /\left(c_{1} D \text { Ro }\right)} ; G$ is the value of parameter $G_{z}$ at $z=h ; h=|L|$.

The velocity $w_{h}$ at the top of the ground layer in Eq. (8) is determined in the following way. Let us calculate $G_{z}$ using Eq. (9), as well as the first term in Eq. (8) at $z=2 h$. Let it be equal to $b_{2 h}$. Then, according to Eq. (8), $\bar{w}(2 h)=b_{2 h}+\bar{w}_{h}$. Since at a small altitudes the profile of $w$ is close to linear, $\bar{w}_{h}=\bar{w}(2 h) / 2$. It follows from the two last relations that: $\bar{w}_{h}=b_{2 h}$.

In the previous studies, 6,7 the following equation for $w(z)$
$w(z)=4 w_{\mathrm{m}} \frac{z}{H_{\mathrm{c}}}\left(1-\frac{z}{H_{\mathrm{c}}}\right)$,
has been widely used when modeling clouds and fogs. In Eq. (1), $H_{c}$ is the level (most often the top of cyclone or anticyclone) where $w$ becomes zero a second time (in addition to the Earth's surface); $w_{\mathrm{m}}$ is maximum (in height) value of $w$ achieved at the level $z_{\mathrm{m}}=H_{\mathrm{c}} / 2$.

Equation (10) was obtained by integration of the continuity equation on the assumption that the divergence of the horizontal wind velocity is a linear function of height.

Figure demonstrates the agreement between the results of $w(z)$ calculations using Eqs. (8)-(9) (solid curves) and those calculated from Eq. (10).

Example I was calculated by Eqs. (8)-(9) at the following values of parameters: Ro $=4 \cdot 10^{4}$, $c_{1} / c_{g}=0.26, \quad z_{0} / z_{1}=0.1, \quad$ and $L / z_{1}=-20 \quad$ (with $\alpha_{0}=34.2^{\circ}, B=2.74, D=0.80$, and $N=4.68 \cdot 10^{-4}$ ). Example II corresponds to $\mathrm{Ro}=4 \cdot 10^{4}, c_{1} / c_{g}=0.39$, $z_{0} / z_{1}=0.1, \quad$ and $L / z_{1}=50$ (here $\alpha_{0}=35.4^{\circ}$, $\left.B=2.93, D=1.98, N=1.87 \cdot 10^{-4}\right)$.


The calculation of $w$ by Eq. (10) was performed on the assumption that the maximum value $w_{\mathrm{m}}$ coincides with the value of $w$ at the top of the boundary layer $\left(w_{\mathrm{m}}=w_{\mathrm{n}}\right)$, while the ratio $H_{\mathrm{c}} / z_{1}=500$.

The vertical velocity calculated by Eqs. (8)-(9) keeps practically the constant value above the boundary layer; Eq. (10) provides for decrease of w in the middle and upper troposphere as the height grows.

In the boundary layer (lower troposphere), the results of the calculation using Eq. (10) agree quite
satisfactory with the data coming from the theory accounting for sufficiently fine features of the boundary layer structure

It follows from the above estimations of $w_{\mathrm{n}}$ that the vertical velocity varies widely under the effect of different parameters $\left(c_{g}, z_{0}, L, c_{1}\right)$. Owing to this, the errors which may arise in w calculation using Eq. (10) because of neglect of some factors (nonstationary motion, for example) will be entirely absorbed by the errors appearing due to the above-mentioned parameters: they are frequently determined in actual practice with a considerable error (the pressure gradient and, especially, $z_{0}$ and $L$ can be, by no means everywhere, retrieved from maps with needed accuracy).

It is not accidental, then, that the results of $w$ calculations using different methods seem to be essentially different (even to the point of signs alternation ${ }^{8}$ ).

In view of these comments, we can conclude that Eq. (10) describes the height distribution of vertical velocity in vortex of synoptic scale with the required accuracy not only in the boundary layer, but throughout the troposphere as well.

## REFERENCES

1. B.E. Peskov, Tr. Tsentral'nogo Instituta Prognozov, issue 136, 61-68 (1964)
2. L.T. Matveev, Meteorol. Gidrol., No. 4, 5-12 (1986).
3. G.I. Morskoi, Meteorol. Gidrol., No. 1, 11-17 (1954).
4. L.T. Matveev, Izv. Akad. Nauk. SSSR, Geofiz., No. 5, 453-461 (1955).
5. L.T. Matveev and Yu.L. Matveev, Izv. Ross. Akad. Nauk, Fiz. Atmos. Okeana, No. 3, 356-362 (1995).
6. L.T. Matveev, Dynamics of Clouds (Gidrometeoizdat, Leningrad, 1981), 311 pp.
7. Yu.L. Matveev, L.T. Matveev, and S.A. Soldatenko, Global Field of Cloudiness (Gidrometeoizdat, Leningrad, 1986), 279 pp.
8. G.I. Morskoi, Tr. Gidromettsentra SSSR issue 30, 82-96 (1968).
